

# Modelling and control summaries



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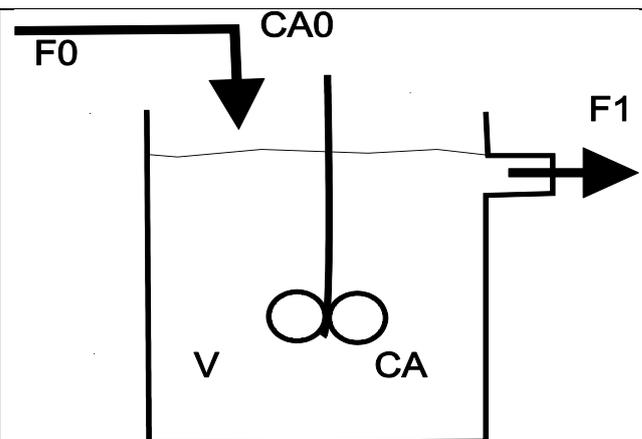
## 1<sup>st</sup> order modelling 9: mixing tank

This note looks at a simple mixing tank system which has flow in at a concentration  $C_{A0}$  and flow out at a different concentration  $C_A$ . The aim is to model how the outlet concentration depends upon the inlet concentration, flow rates and tank volume.

### ASSUMPTIONS

1. For simplicity here we assume that the flow in  $F_0$  and the flow out  $F_1$  are equal. This means the volume  $V$  in the tank is fixed.
2. The tank is well mixed so the concentration in the tank matches the outlet concentration.
3. The solvent and product A have the same density.
4. There is no reaction in the tank involving A.

**MODELLING** is done using a **mass or molar balance** (these are equivalent). To be more precise, we balance the rate of change of mass A within the tank.



### MASS BALANCE

**Accumulation of A = A (input) – A (output) + generation of A – expenditure of A**

Note that the assumption here is that generation and expenditure (say from reactions) are zero.

DEFINE  $M_A$  as mass per mole for pure A, so mass of A per  $m^3$  within solvent is  $C_A M_A$

- The rate of A coming into the tank is determined by inlet flow  $F_0$  and inlet concentration.  
Mass flow rate in =  $F_0 C_{A0} M_A$
- The rate of A leaving the tank is determined by outlet flow  $f_1$  and outlet concentration.  
Mass flow rate out =  $F_1 C_A M_A$
- The total mass in the tank =  $V C_A M_A$  so, given  $V$  and  $M_A$  are constant. Therefore the rate of change of mass in the tank is given by

$$VM_A \frac{dC_A}{dt} = (M_A F_0 C_{A0} - M_A F_1 C_A)$$

It is noted that the term  $M_A$  is a common factor throughout and so can be removed. Also, the assumption is that  $F_1 = F_0 = F$  and hence:

$$\left\{ V \frac{dC_A}{dt} = (F C_{A0} - F C_A) \right\} \equiv \left\{ \underbrace{\left( \frac{V}{F} \right)}_T \frac{dC_A}{dt} + C_A = \underbrace{1}_{\text{gain}} \times C_{A0} \right\}$$

1. Because there is no reaction, the steady-state gain is clearly one, that is the concentration in the tank tends to the concentration of the input flow.
2. The time constant increases if the volume increases and decreases if the flow increases. Both of these should be intuitively obvious.

### Numerical example

Find the response of a mixing tank with the following data and subject to a step increase in  $C_{A0}$  of magnitude  $0.925 \text{ mole/m}^3$ .

$F=0.085 \text{ m}^3/\text{min}$ ;  $V=2.1 \text{ m}^3$ ;  $C_A(0)=0.925 \text{ mole/m}^3$ ;  $C_{A0}=0.925 \text{ mole/m}^3$

Assume the system is initially at steady state before the step change in  $C_{A0}$ .

ANSWER:

1. First note that the effective inlet concentration is now  $C_{A0}=1.85$  as the data gives an increase from the current value.
2. The effective initial condition  $C_A(0)$  for the outlet concentration is  $0.925$  as the system begins from steady-state.
3. In standard time constant form, the model and data are:

$$\left\{ \left( \frac{V}{F} \right) \frac{dC_A}{dt} + C_A = \underbrace{1}_{\text{gain}} \times C_{A0} \right\}; \quad C_A(0) = 0.925, \quad C_{A0} = 1.85, \quad \frac{V}{F} = \frac{2.1}{0.085} = 24.7$$

Consequently, using standard responses for a 1<sup>st</sup> order model:

$$C_A(t) = 0.925 + 0.925(1 - e^{-\frac{t}{24.7}})$$

### Summary

1. Derived model for a simple mixing tank, with and without deviation variables.
2. Model is linear and takes a standard 1st order format.
3. Time constant linked to tank volume and flow rate.
4. Steady-state gain is unity as there is no consumption or production.